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HADAMARD SOURCE ENCODING TECHNIQUES APPLIED TO APOLLO TELEMETRY LINKS: AN EVALUATION

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ABSTRACT

The effort described in this paper is an investigation of the possible improvement in performance of the Apollo Unified S-Band Telemetry links due to the use of the Hadamard transform as a means of source encoding. Both rapidly and slowly varying telemetry signals were considered and three sizes of the Hadamard matrix were used. Results indicate that as much as 3-db improvement in system performance may be obtained in systems operating at a 2% RMS error level.

INTRODUCTION

In recent years, the practicality of space communications, both for manned space research and unmanned communications satellites, has become evident. The rapidly increasing amount of information to be transmitted is placing arduns demands on the system channel capacity demands on the system channel capacity space probes requires improved system space probes requires improved system signal-to-noise ratios. Data compression and channel encoding techniques have been developed to help meet these more rigid requirements [1], [2].

Recent developments of "fast" orthogonal transforms have provided new concepts of source encoding as a means of reducing bandwidth and carrier-power requirements for space communication systems. Some of the more promising transforms include the Fourier, Haar, Hadamard and Karhunin-Loeve transforms, [3], [4], [5].

The effort described in this paper is an investigation of the possible improvement of the Apollo Unified S-Band Telemetry Links due to the use of the Hadamard transform as a means of source encoding. Actual command and service module-ground station communication equipment with a simulated RF link was used in the test. These facilities are located at the Manned Spacecraft Center. Both slowly changing and rapidly changing digital signals were

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investigated. Hadamard matrices of orders 4, 16, and 64 were used in obtaining the transformations.

It is realized that the resulting system is not "optimal" in any manner, but the results do reflect the advantages of using the Hadamard technique without redesign of other system components. Areas where system changes could result in significant additional improvement in performance are also revealed.

Section II gives a brief summary of the Hadamard transform. The experimental study is described in Section III. The results of this study are shown in Section IV and conclusions are presented in Section V.

THE HADAMARD TRANSFORM

Given a one dimensional signal, f(t), its finite sampled transform can be represented as

$$Y = HX$$
 (1)

where X is an N x l vector of signal samples of f(t), H is an N x N transformation matrix and Y is an N x l vector of transformed samples. One element of Y is

$$Y(n) = \sum_{k=0}^{N-1} x (k\Delta T) h_{kn}$$
(2)

For orthogonal transforms, the signal vector elements are recovered by

$$X(k\Delta T) = \sum_{n=0}^{N-1} Y(n) h_{kn}$$
(3)

In eqs. (2) and (3), h_{kn} is an element of the matrix H. If the element h_{kn} is defined as the inner product

$$h_{kn} = \langle Wal(k, \xi), \delta(\xi - \frac{n}{NAT}) \rangle$$
 (4)

then the resulting matrix is the Hadamard matrix and the transformation is known as

the Hadamard Transform. In eq. (4), the Wal (k,8) represent the set of Walsh functions, the first eight of Walsh functions, the first eight of Walsh Functions, the first eight of Walsh resolvent eight of Walsh eight eight

Except for a constant factor equal to the rank of the matrix, the Hadamard matrix is its own inverse. Thus, to recover the original vector X:

$$x = H^{-1} \quad Y = \frac{1}{N} HY$$

This expression is signigicant from the standpoint that implementation of the Hadamard transform technique requires development of only one piece of hardware for both the transform and inverse transform processes.

The most significant advantage of the Hadamard matrix, however, is its ability to effect a transform of a signal while requiring only the operations of additions and subtractions.

EXPERIMENTAL STUDY

The system diagram for this study is shown in Figure 3. One-hundred ninety-six signal samples were generated to correspond to the command and service module low bit rate telemetry format of 200 words which includes four frame synchronization words. Two types of signal samples were generated. The first type consisted of 196 samples evenly spaced over one cycle of a sine aware. This signal was chosen to represent battery voltage, vehicle velocity, etc. The second signal type was 196 data points chosen by sampling a random variable uniformly distributed over the interval (0,1). This type of course represents rapidly or randomly changing telemetry signals.

The signals were processed in three phases. The first phase was accomplished on the Univac 1108 Computing System and consisted of signal generation, Hadamard transformation of the signal if applicable, and pulse code modulation (PCM) of the transformed and untransformed signals. An eight bit uniform quantization method was used for the PCM. This was accomplished by generating 256 evenly spaced levels between the maximum and minimum values of input data and then assigning each data

point to the closest level. Hence for each data point, an 8-bit binary number between 0 and 255 is generated. The sequence of 196 eight-bit numbers and four eight-bit synch words from one 1600 bit frame. This frame is supplied to the second phase of the system which is detailed in Figure 4.

Actual spacecraft-ground station communication equipment was used in phase two. The RF path from spacecraft to ground station was of course simulated but is accurately calibrated so that the simulation closely resembled actual mission conditions. Data was transmitted for three different system bit error rates (BER). Ten thousand frames (16 million bits) were examined for 10-4 BER; 5000 frames for 10-3 BER; and 1000 frames for 10-2 BER. The FCM bit synchronizer output was recorded on magnetic tape for use in phase three.

The Univac 1108 computer was again utilized in the last step of the signal processing. Using the reference levels from phase I, the PCM signal recorded in phase II was decoded and the inverse transformation performed if necessary. The resulting estimates of the original signal were then compared with the actual values and the per cent RMS error rate per word was calculated.

For a standard of comparison, the signals were processed in the normal manner through the system and the RMS error calculated. The signals were then Hadamard transformed and processed in the same manner. Three sizes of the matrix (N=4, N=16, N=64) were considered in each case. Hence, a total of eight different bit streams were transmitted for each of the three bit error rates.

RESULTS

Per cent RMS error vs bit error rate for slowly changing (sine wave) data is shown in Figure 5. Two cases are depicted; untransformed data and data transformed by the Hadamard technique with N=4. The data from runs with N=16 and N=64 were so close to the N=4 case as to be indistinguishable on a graph. Surprisingly, the N=16 and N=64 data were slightly worse than the N=4 case.

Figure 6 depicts the RMS error comparison for the fast changing (random) input signal. Again the N=16 and N=64 cases were very close, but slightly worse than for N=4.

Curves relating bit error rate and signalto-noise ratio for PSK matched filter detection are well established [6]. Hence, using this known relation and the information from Figures 5 and 6, one can construct the comparison shown in Figure 7. Improvement of system performance in db is plotted as a function of 8 RMS error. For example, if the system normally operates at a 28 RMS error level and slowly varying data is considered, then the required system signal-to-noise ratio can be reduced 2.8 db by using the Hadamard transform technique.

It is significant to note in Figures 5 and 6 that at low bit error rates (= 10-4) the conventional system outperforms the Hadamard system. This phenomenon can be attributed to the quantization scheme used. It is possible to show that the quantization error for the Hadamard system is equal to the quantization error of the conventional system plus a positive quantity that is a function of system parameters. Hence, for low bit errors when quantization noise becomes significant the performance of the Hadamard system should be worse. However, as the bit error rate increases and the channel noise becomes the major contributor to RMS error, the noise distributing properties of the Hadamard transform provides significant improvement and the overall performance of the Hadamard system as compared to the conventional system increases.

Also the RMS error of the Hadamard system increases as the matrix size N increases if there is no channel noise (S $|N=\infty|$). This may explain why the performance of the N=16 and N=64 cases were slightly worse than the N=4 case.

CONCLUSIONS

It has been shown experimentally that Hadamard transform techniques can provide significant improvement in Apollo Unified S-Band System performance, especially if the input data is changing slowly. However, for low bit error rates uniform quantizing, the conventional system is better. The study was made under the constraint that no changes be made in the existing Apollo System except the introduction of the transform itself. It is felt that significant additional improvement could be obtained using other more nearly optimum quantizing schemes.

As a sidelight, it was noted that a 4:1 data compression could be accomplished by transmitting only transform values greater than zero (approximately) and the position of these values.

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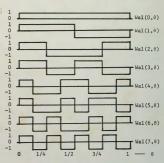
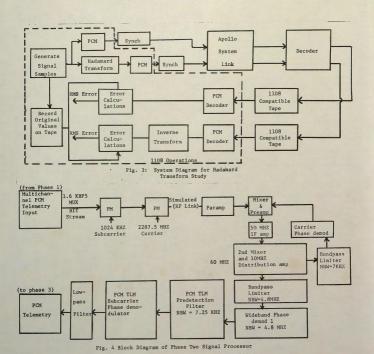


Fig. 1 First Eight Walsh Functions

Fig. 2 Examples of Hadamard Matrices



10-4

